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<u>L24</u>	114 and L23	2	<u>L24</u>
<u>L23</u>	324/?.ccls. or 322/?.ccls. or 375/?.ccls. or 307/?.ccls. or 702/?.ccls. or 701/?.ccls.	8615	<u>L23</u>
<u>L22</u>	114 and L21	0	<u>L22</u>
<u>L21</u>	(3893007 3857043 3735220 3365614).pn.	.11	<u>L21</u>
<u>L20</u>	(3440433 3546548 3365614 3893007 3735220 3527991 2668247 3577001 3857043 3716768)![PN]	36	<u>L20</u>
<u>L19</u>	('4090114' '4209816')[PN]	4	<u>L19</u>
<u>L18</u>	114 and L17	0	<u>L18</u>
<u>L17</u>	(6900618 6809428 6734577 6717384 6707278 6426609 6215285).pn.	16	<u>L17</u>
<u>L16</u>	('4090114' '4636706' '4209816')[URPN]	79	<u>L16</u>
<u>L15</u>	(conver\$ adj frequency) near (rpm adj (value or signal))	0	<u>L15</u>
<u>L14</u>	112 and L13	17	<u>L14</u>
<u>L13</u>	ac or (alternate adj 1 current)	796991	<u>L13</u>
<u>L12</u>	110 and L11	21	<u>L12</u>
<u>L11</u>	dc or (direct adj1 current)	890260	<u>L11</u>

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<u>L12</u>	110 and L11	21	<u>L12</u>
<u>L11</u>	dc or (direct adj1 current)	890260	<u>L11</u>
<u>L10</u>	18 and L9	28	<u>L10</u>
<u>L9</u>	frequency or spectrum	2192398	<u>L9</u>
. <u>L8</u>	16 and L7	36	<u>L8</u>
<u>L7</u>	(filter\$3 or separat\$) near3 signal	292920	<u>L7</u>
<u>L6</u>	11 and 12 and L5	231	<u>L6</u>
<u>L5</u>	13 same L4	7301	<u>L5</u>
<u>L4</u>	sens\$3	2472649	<u>L4</u>
<u>L3</u>	electric\$2 adj 1 system	60415	<u>L3</u>
<u>L2</u>	vehicle	1919889	<u>L2</u>
<u>L1</u>	rpm or (revolution adj2 minute)	272886	<u>L1</u>

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<u>L7</u>	(filter\$3 or separat\$) near3 signal	292920	<u>L7</u>
<u>L6</u>	11 and 12 and L5	231	<u>L6</u>
<u>L5</u>	13 same L4	7301	<u>L5</u>
<u>L4</u>	sens\$3	2472649	<u>L4</u>
<u>L3</u>	electric\$2 adj1 system	60415	<u>L3</u>
<u>L2</u>	vehicle	1919889	<u>L2</u>
<u>L1</u>	rpm or (revolution adj2 minute)	272886	<u>L1</u>

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<u>L9</u>	frequency or spectrum	2192398	<u>L9</u>
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<u>L7</u>	(filter\$3 or separat\$) near3 signal	292920	<u>L7</u>
<u>L6</u>	11 and 12 and L5	231	<u>L6</u>
<u>L5</u>	13 same L4	7301	<u>L5</u>
- <u>L4</u>	sens\$3	2472649	<u>L4</u>
<u>L3</u>	electric\$2 adj1 system	60415	<u>L3</u>
<u>L2</u>	vehicle	1919889	<u>L2</u>
· <u>L1</u>	rpm or (revolution adj2 minute)	272886	<u>L1</u>

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<u>L7</u>	(filter\$3 or separat\$) near3 signal	292920	<u>L7</u>	
<u>L6</u>	11 and 12 and L5	231	<u>L6</u>	
<u>L5</u>	13 same L4	7301	<u>L5</u>	
<u>L4</u>	sens\$3	2472649	<u>L4</u>	
<u>L3</u>	electric\$2 adj1 system	60415	<u>L3</u>	
<u>L2</u>	vehicle	1919889	<u>L2</u>	
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<u>L17</u>	(6900618 6809428 6734577 6717384 6707278 6426609 6215285).pn.	16	<u>L17</u>
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<u>L15</u>	(conver\$ adj frequency) near (rpm adj (value or signal))	0	<u>L15</u>
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<u>L13</u>	ac or (alternate adj 1 current)	796991	<u>L13</u>
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<u>L10</u>	18 and L9	28	<u>L10</u>
<u>L9</u>	frequency or spectrum	2192398	<u>L9</u>

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(conver\$ adj frequency) near (rpm adj (value or signal))	0

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<u>L2</u>	vehicle	1919889	<u>L2</u>

<u>L1</u> rpm or (revolution adj2 minute)

272886 <u>L1</u>

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Jun 24, 1980

DOCUMENT-IDENTIFIER: US 4209816 A

TITLE: Protective control for vehicle starter and electrical systems

Abstract Text (1):

A protective control for the starter and electrical systems of a motor vehicle, including a main relay for controlling the electrical system, and a starter relay for controlling the starter system. Electronic logic is provided for the electrical system which: (1) prevents energization of the main relay if the battery polarity is reversed; (2) if the battery polarity is correct, turns on the main relay when a master switch is closed; and (3) maintains the main relay in an ON condition when an AC signal from the alternator is sensed even if the masterswitch is subsequently opened. The latter prevents disconnection of the battery from the electrical system while the engine is running. Electronic logic is also provided for the starter relay which: (1) after the main relay is closed, turns on the starter relay when a starter switch is closed, to thus permit cranking of the engine; (2) automatically deenergizes the starter relay when the AC signal from the alternator attains a designated threshold frequency, which corresponds to a pre-determined engine $\underline{\mathtt{RPM}}$ at which it is desired to disengage the starter; and (3) has a hysteresis network to prevent subsequent re-energization of the starter relay until the AC signal from the alternator drops to a value substantially below the original threshold frequency, preferably when the engine is stopped or almost stopped, whereby the starter switch will re-energize the starter relay only if the master switch is closed and the engine is not running.

Brief Summary Text (2):

Protective systems for starter mechanisms in motor <u>vehicles</u> are known in the art. Protection is desirable in order to prevent damage which may otherwise occur if the starter is overrun, or re-energized after the engine is running. Starter protector or lock-out systems typically sense some function of engine <u>RPM</u> during the starter sequence and automatically remove electrical power to the starter motor when the engine attains an adequate <u>RPM</u> level to be running. Starter disconnect circuits are known which respond to intake manifold vacuum, oil pressure, <u>frequency of an AC</u> generator voltage, etc., to disable the starter at a predetermined engine <u>RPM</u>.

Brief Summary Text (5):

The present invention relates to an improved starter protector, and also to the combination thereof with a control for the <u>vehicle</u> electrical system.

Brief Summary Text (6):

An object of the invention is to provide an improved protective control for <u>vehicle</u> starter systems which senses alternator <u>frequency</u> as a measure of engine <u>RPM</u> and automatically deenergizes the starter relay above a given threshold <u>frequency</u> and in which such <u>frequency</u> selective circuit includes a hysteresis network also responsive to alternator <u>frequency</u> to prevent subsequent re-energization of the starter until a reduced engine RPM.

Brief Summary Text (7):

Another object of the invention is to provide a starter protector of the aforementioned character in combination with an electrical system control having a master switch for connecting the <u>vehicle</u> battery to the starter system and to the electrical system, and having signal detection means also responsive to the alternator to prevent disconnection of the battery while the engine is running even if the master switch is subsequently opened.

Brief Summary Text (9):

Another object of the invention is to provide a protective control of the aforementioned character having a <u>frequency</u> selective circuit responsive to alternator <u>frequency</u> for not only locking-out the starter at a selected threshold <u>frequency</u> but also including a hysteresis

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network for preventing re-energization of the starter above a lower selected frequency.

Brief Summary Text (10):

Another object is to provide a protective control of the aforementioned character wherein both the threshold and the lower selected frequencies are adjustable.

Brief Summary Text (11):

Another object of the invention is to provide a protective control of the aforementioned character exhibiting excellent thermal stability of the threshold frequency lockout set point.

Brief Summary Text (12):

Another object of the invention is to provide a protective control of the aforementioned character having a substantially widened range of frequency hysteresis.

Brief Summary Text (13):

Another object of the invention is to provide a protective control of the immediately aforementioned character utilizing an integrated circuit for threshold frequency selection.

Brief Summary Text (14):

Another object of the invention is to provide a protective control of the immediately aforementioned character having an add-on hysteresis network affording a wider range of hysteresis; and thus a substantially lower reset frequency point, than available solely from a resistor connection between a designated two of the integrated circuit's pins.

Brief Summary Text (16):

Another object of the invention is to provide a protective control of the aforementioned character having an input waveshaping circuit to compensate for the poor waveform shape, variable amplitude, and associated electrical extraneous noise in the AC voltage signal from the alternator.

<u>Detailed Description Text</u> (3):

There is shown in FIG. 1 a protective control module outlined by a box 22, for use in a motor vehicle. The module includes a main relay 24 and a starter relay 26. The main relay is used to connect the vehicle battery 28 to the vehicle electrical system, generally designated 30. The starter relay is used to control the engine starter motor 32, and is connected to the starter solenoid 34.

Detailed Description Text (4):

The main relay and the starter relay are each controlled by respective electronic logic circuits 36 and 38 which are responsive to the AC voltage output signal of alternator 40. The alternator is driven by the engine, and thus the presence of an output signal from the alternator indicates that the engine is running, and the frequency of the AC voltage signal is a function of engine RPM.

<u>Detailed Description Text</u> (5):

Logic circuit 36 permits energization of main relay 24 when master switch 42 is manually closed by the driver, enabling current to flow to coil 24a which then pulls in armature 24b downwardly to complete a circuit from battery 28 to electrical system 30. Logic circuit 36 includes signal detection means, to be more fully described hereinafter, which senses the presence of a signal from alternator 40 and will hold the main relay closed even if the master switch is subsequently opened. This prevents disconnection of battery 28 from electrical system 30 while the engine is running. When no alternator signal is present, master switch 42 can open as well as close main relay 24.

Detailed Description Text (6):

Logic circuit 38 permits energization of starter relay 26 when main relay 24 is closed and starter switch 44 is manually closed by the driver, enabling current to flow to coil 26a which then pulls in armature 26b downwardly to complete a circuit from battery 30 through main relay 24 through starter relay 26 to starting motor solenoid 34, and hence enabling cranking of the engine by starting motor 32. Logic circuit 38 includes frequency selective means, to be more fully described hereinafter, which senses the frequency of the AC output signal from alternator 40 and responds to a predetermined set threshold cut-out frequency by automatically terminating current flow to coil 26a thus de-energizing starter relay 26 and breaking the circuit to solenoid 34, hence disengaging the starter. The set threshold cut-out frequency corresponds to

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a designated engine RPM beyond which the engine should not be cranked by starter motor 32. The frequency selective means of logic circuit 38 also includes hysteresis means which prevents subsequent re-energization of starter relay 26 until the AC signal frequency drops to a substantially lower reset cut-in frequency, preferably near zero, so that the engine cannot be cranked again until its RPM is low enough that the solenoid drive teeth, flywheel teeth, etc. will not be damaged.

Detailed Description Text (8):

The particular module disclosed was specifically designed for use in military vehicles, though the invention is of course not limited thereto. The module is compact, measuring 71/2 inches long by 31/2 inches wide by 31/2 inches high, and is an easy to install component. Terminal A is connected through master switch 42 to the positive side of battery 28. Terminal C is connected to the positive side of battery 28. Terminal D is connected to alternator 40 and to the vehicle electrical system, 30 in FIG. 1. Starter switch 44 is connected between terminals D and E. Terminal B is connected to starting motor solenoid 34. Terminal F is connected to the alternator to sense the AC output signal thereof; this AC signal is typically available as a special tap internal to the alternator on the AC side of the rectifier diodes.

Detailed Description Text (10):

Dashed box 46 outlines a voltage regulation circuit comprising the combination of dropping resistor 48 and zener diode 50 used in the particular disclosed embodiment to drop the military vehicle 24 volt DC power down to a regulated 12 volt DC level supply for the precision frequency selective circuitry, to be described hereinafter.

Detailed Description Text (11):

Dashed box 52 outlines an input waveshaping circuit. The AC signal supplied by the alternator does not have a clean waveshape, and it varies in magnitude, particularly during the starting interval with which the present invention is concerned. A resistor 54 limits current to the base of an NPN transistor 56 and also forms an RC noise filter with a capacitor 58 connected across the base and emitter of transistor 56. The alternator signal is fed via terminal F through this network to the base of transistor 56 which is switched on and off by the signal. The collector of transistor 56 switches on and off (low and high) on the leading and trailing edges of the signal to the base, providing a pulse shaped signal of constant amplitude which is more suitable to be fed to the <u>frequency</u> selective circuitry, to be described hereinafter. Resistor 60 is connected in parallel with capacitor 58 across the transistor base-emitter to provide a base to emitter return path to aid turn-off. Resistor 62 is a collector load, or pull-up, resistor and is connected between the transistor collector and voltage regulation circuit 46. Capacitor 64 and resistor 66 provide coupling from the transistor collector signal to the frequency selective circuit.

Detailed Description Text (12):

Dashed box 68 outlines a frequency selective circuit. This circuit includes 3344 type integrated circuit, designated by the reference character 70. The same pin designations assigned to a 3344 type integrated circuit are used in FIG. 2 to facilitate clarity of the description to follow. The other components in frequency selective circuit 68 will be identified in the continuing description.

Detailed Description Text (13):

The pulse waveform from the collector of transistor 56 is fed to input pin 11 of component 70, and an output \underline{DC} signal is derived at pin 3. Pin 3 is high or ON as long as the incoming frequency at pin 11 is below a predetermined set point or threshold_frequency, which in this particular embodiment is 127 Hz. As the engine is started and its RPM's increase to a running or idling level, the frequency of the sensed alternator signal reaches 127 Hz at which point pin 3 now goes low or OFF, removing bias to the base of transistor 72 which in turn causes disengagement of starter relay 26, to be more fully described hereinafter. The frequency of the switch point is determined by the values of resistors 74 and 76 and capacitor 78. A stable metal glaze resistor is used for 74 and a polycarbonate capacitor for 78 to provide excellent frequency stability for the cut-out switch point of 127 Hz. This switch point remained within .+-.2 Hz over the temperature range -65.degree. F. to +250.degree. F. Component 70 itself is very stable but is at the mercy of the external threshold frequency determining elements.

Detailed Description Text (14):

A frequency hysteresis network, outlined in dashed box 80, is added in frequency selective

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circuit 68 such that once the trip out frequency at pin 11 has been attained or exceeded, the input frequency at pin 11 must now drop down substantially below said threshold trip out frequency before the starter relay can be re-energized (by pin 3 going back high), thus assuring starter lockout until the engine is essentially stopped. The hysteresis drops the reset frequency to below 10 Hz in this particular embodiment. This is accomplished by transistor 82 in conjunction with resistors 84 and 86 and capacitor 88, and a switching signal from pin 5 of component 70. When the frequency of the input signal to pin 11 is below the threshold trip frequency, 127 Hz, pin 5 is low or OFF, but when the input signal on pin 11 reaches 127 Hz, pin 5 switches high (the opposite or complement of output pin 3). When pin 5 toggles high, the base of transistor 82 is biased on through resistor 84. The collector of transistor 82 goes low, effectively grounding one side of capacitor 88, whereby the latter now is in effect in parallel with capacitor 78. (When the collector of transistor 82 is high, capacitor 88 is merely floated.) The addition of capacitor 88 in the frequency determining network of component 70 drops the switching frequency down to below 10 Hz. Once below this reset point, the threshold trip frequency will again recover to 127 Hz, allowing a normal restart of the engine. It is thus seen that when the input frequency at pin 11 reaches 127 Hz, pin 3 toggles low to disengage the starter and pin 5 toggles high to drop the reset frequency down to below 10 Hz. Pin 3 remains low until the input frequency at pin 11 decreases to less than 10 Hz, at which point pin 3 toggles back high (pin 5 goes low) to thus bias on transistor 72 whereby starter relay 26 may be re-energized and the engine cranked again.

Detailed Description Text (15):

A type 3344 integrated circuit, component 70, has provisions for obtaining hysteresis of input frequency by merely adding a resistor 90 between pins 10 and 12, but the range between initial and reset frequency set points, without adversely affecting circuit operation, was not as wide as preferred. Thus the hysteresis network 80 with transistor 82 switching in capacitor 88 was added, and was very effective. Since the low, or reset, frequency point is not critical compared to the initial threshold set frequency point, the requirements for capacitor 88 stability are not as great as for capacitor 78.

Detailed Description Text (16):

Other components in <u>frequency</u> selective circuit 68 include resistor 92 which limits the output current from pin 3 to the base of transistor 72, and capacitor 94 which is part of an additional integrator network used in the operation of integrated circuit 70.

Detailed Description Text (17):

Dashed box 96 outlines a starter relay drive circuit. The output switching signal from pin 3 of component 70 is supplied to the base of a darlington power transistor 72 which functions as an amplifier switch for starter relay coil 26a. When starter switch 44, FIG. 1, is closed, 24 volts DC is supplied to terminal E, FIG. 2, and starter relay 26 will be energized, whereby the engine is cranked. When the engine attains a predetermined RPM level, as indicated by the alternator supplying 127 Hz to the circuit at terminal F, the starter relay will be deenergized by transistor 72 turning off in response to pin 3 going low. The starter relay 26 will remain de-energized, even if starter switch 44 is held closed or re-closed, until the alternator signal drops below 10 Hz, whereby the engine cannot be cranked again until it has essentially stopped.

Detailed Description Text (20):

Signal detector circuit 108 rectifies and filters the AC alternator signal, supplied to terminal F, through diode 112 and capacitor 114 and forms a DC voltage to bias ON darlington power transistor 116. Normally, when the engine is not running, master switch 42 will supply battery power to terminal A and will thus energize main relay 24 by supplying bias to the base of transistor 116 through resistor 118, and supplying coil bias through diode 120. Conduction of transistor 116 completes a circuit from terminal A through main relay coil 24a through transistor 116 to ground, whereby master switch 42 can thus turn main relay 24 on and off. However, once the engine is running and the alternator signal correspondingly supplied to signal detector circuit 108, transistor 116 will be biased ON even if master switch 42 is opened; in such case, coil 24a bias is supplied from terminal D through diode 106. Consequently, main relay 24 will remain closed until the alternator signal ceases, i.e. the engine stops. In the particular application of the preferred embodiment, the engine is not supposed to be stopped by the master switch, but by a fuel shut-off valve commonly used in diesel engined vehicles.

<u>Detailed Description Text</u> (25):

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The <u>vehicle</u> operator first closes master switch 42, FIG. 1, thus supplying battery power to terminal A. If the battery polarity is correct, main relay 24 will close due to the bias to coil 24a through diode 120 and transistor 116, FIG. 2. If the battery polarity is reversed, main relay 24 will not close because diode 120 is then blocking and prevents application of power to coil 24a; no circuit damage occurs because the electrical system cannot be connected, nor can starter relay 26 be energized.

Detailed Description Text (26):

With correct battery polarity and main relay 24 closed, battery 28 is tied into the <u>vehicle</u> electrical system by armature 24b closing the contacts between terminals C and D, FIG. 1. At this time master switch 42 has full control of main relay 24 and can open the latter if desired.

Detailed Description Text (27):

With the <u>electrical system</u> now energized, the operator can start the engine by closing starter switch 44, FIG. 1, supplying power from terminal D to terminal E. Starter relay 26 will now be energized because transistor 72, FIG. 2, is biased ON by a signal from output pin 3 of component 70 which in turn has <u>sensed</u> at input pin 11 that no signal yet exists from the alternator at terminal F. The engine will now be cranked by starter motor 32, FIG. 1, because of the energization of solenoid 34 enabled by the completed circuit therethrough from closed starter relay 26.

Detailed Description Text (28):

As the engine begins to pick up speed, its <u>RPM</u> level increases such that alternator 40, FIG. 1, will generate a signal at its <u>AC</u> internal tap, which <u>AC</u> signal is fed to terminal F on control module 22. The <u>AC</u> signal <u>frequency</u> is proportional to engine <u>RPM</u>, and when the <u>frequency</u> reaches a predetermined set point value, here 127 Hz, <u>frequency</u> selective circuit 38 in FIG. 1, 68 in FIG. 2, ceases bias to starter relay drive circuit 96, thus dropping out or opening starter relay 26 (unless of course the starter relay has already been opened by the operator's opening of starter switch 44). The starter function is now locked out and starter switch 44 is ineffective until the alternator's <u>AC</u> signal <u>frequency</u> is very low due to the hysteresis provided in <u>frequency</u> selective circuit 68 by <u>frequency</u> hysteresis network 80, FIG. 2, after trip out. The low level reset point in this case is 10 Hz, whereby the engine must be essentially stopped before it can be re-cranked.

<u>Detailed Description Text</u> (29):

While the engine is running and the alternator signal is supplied to terminal F of the module, the master switch 42 can be opened but the main relay 24 will remain closed due to the signal detector circuit 108, FIG. 2, maintaining bias on main relay driver circuit 110. Main relay 24 can only be opened when the engine RPM is very low such that the alternator signal ceases.

CLAIMS:

1. A protective control for the starter system of an engine which is cranked by a starter motor, comprising:

starter relay means in circuit with said starter motor;

 $\underline{\text{frequency}}$ selective means responsive to engine $\underline{\text{RPM}}$ to automatically open said starter relay means above a predetermined threshold set $\underline{\text{frequency}}$ corresponding to a designated $\underline{\text{RPM}}$ level, to prevent cranking of said engine thereabove,

said <u>frequency</u> selective means including hysteresis means to prevent reclosing of said starter relay means until engine <u>RPM</u> drops to a lower level corresponding to a reset <u>frequency</u> less than said threshold set <u>frequency</u>, whereby to prevent recranking of said engine until engine <u>RPM</u> drops to said lower level;

transducer means responsive to engine speed to produce a signal whose <u>frequency</u> corresponds to engine RPM,

said <u>frequency</u> selective means having an input for receiving said transducer signal and an output controlling said starter relay means;

wherein said transducer signal, upon reaching said threshold set frequency, causes said output

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to switch states and also activates said hysteresis means to lower the frequency value necessary to cause switching of said output back to its original state;

said transducer means comprising an AC signal generator and input waveshaping means for receiving the AC signal and delivering a clear waveshape signal to said input of said frequency selective means;

said frequency selective means comprising a programmable frequency switch having an input receiving said transducer signal and a pair of opposite state outputs one of which is connected to said starter relay means and the other of which is connected to a hysteresis network, such that when the frequency of said transducer signal at said input reaches said threshold value, said outputs switch states such that said one output causes opening of said starter relay means and said other output causes said hysteresis network to lower the value of said threshold frequency down to said reset frequency;

said hysteresis network comprising a capacitor which is floated when the other of said outputs is in the first mentioned of its states, and which is connected in circuit with said frequency switch when said other of said outputs switches to its second mentioned state.

- 3. The invention according to claim 1 wherein said frequency selective means comprises a second capacitor connected to another input of said frequency switch for selecting the value of said threshold set frequency, said first capacitor being connected in parallel with said second capacitor when said other output is in said second state, said parallel combination of said capacitors determining the value of said reset frequency.
- 4. The invention according to claim 1 wherein said transducer comprises an alternator driven by said engine, and wherein said input waveshaping means comprises a transistor biased by the AC alternator signal to abruptly switch ON and OFF on leading and trailing edges of said AC signal, one of the emitter and collector of said transistor thus switching low and high and connected to said input of said frequency selective means for delivering a clean pulse shape signal thereto.
- 5. A protective control for the starting and electrical systems of a vehicle having an engine which is cranked by a starter motor and battery, comprising:
- a main relay between said battery and said electrical system:
- a starter relay between said main relay and said starter motor;
- a master switch in circuit with said main relay;
- a starter switch in circuit with said starter relay;
- electronic logic for said main relay which:
- (a) permits energization of said main relay when said master switch is closed; and
- (b) senses engine RPM and will maintain said main relay closed even if said master switch is subsequently opened, whereby to prevent disconnection of said battery from said electrical system when said engine is running;

electronic logic for said starter relay which:

- (a) after said main relay is closed, permits energization of said starter relay when said starter switch is closed, to thus enable energization of said starter motor and cranking of said engine;
- (b) senses engine RPM and automatically de-energizes said starter relay at a predetermined set threshold engine RPM level to thus disengage said starter motor; and
- (c) prevents subsequent re-energization of said starter relay and hence said starter motor until engine RPM drops to a reset level lower than said predetermined set threshold level;

transducer means responsive to engine speed to produce a signal whose frequency corresponds to

engine RPM,

said electronic logic for said starter relay comprising <u>frequency</u> selective means having an input for receiving said transducer signal and an output controlling said starter relay;

said <u>frequency</u> selective means including hysteresis means such that said transducer signal upon reaching a predetermined set threshold <u>frequency</u> corresponding to said set threshold engine <u>RPM</u> level causes said output to switch states to de-energize said starter relay and also activates said hysteresis means to lower the input <u>frequency</u> necessary to switch said output back to its original state down to a reset <u>frequency</u> value less than said set threshold <u>frequency</u> and corresponding to said reset lower level engine <u>RPM</u>, said electronic logic for said main relay responding to the same said transducer signal for sensing engine <u>RPM</u>.

- 6. The invention according to claim 5 wherein said transducer comprises an \underline{AC} signal generator, said invention further comprising input waveshaping means for receiving the \underline{AC} signal and delivering a clean waveshape signal to said input of said $\underline{frequency}$ selective means.
- 7. The invention according to claim 6 wherein said transducer comprises an alternator driven by said engine, and wherein said input waveshaping means comprises a transistor biased by the \underline{AC} alternator signal to abruptly switch ON and OFF on leading and trailing edges of said \underline{AC} signal, one of the emitter and collector of said transistor thus switching low and high and connected to said input of said $\underline{frequency}$ selective means for delivering a clean pulse shape signal thereto.
- 8. The invention according to claim 5 wherein said <u>frequency</u> selective means comprises a programmable <u>frequency</u> switch having an input receiving said transducer signal and a pair of opposite state outputs one of which is connected to said starter relay the other of which is connected to a hysteresis network, such that when the <u>frequency</u> of said transducer signal at said input reaches said set threshold value, said outputs switch states such that said one output causes opening of said starter relay and said other output causes said hysteresis network to lower the value of said threshold <u>frequency</u> down to said reset <u>frequency</u>.
- 9. The invention according to claim 8 wherein said hysteresis network comprises a capacitor which is floated when the other of said outputs is in the first mentioned of its states, and which is connected in circuit with said <u>frequency</u> switch when said other of said outputs switches to its second mentioned state.
- 11. The invention according to claim 9 wherein said <u>frequency</u> selective means comprises a second capacitor connected to another input of said <u>frequency</u> switch for selecting the value of said threshold set <u>frequency</u>, said first capacitor being connected in parallel with said second capacitor when said other output is in said second state, said parallel combination of said capacitors determining the value of said reset frequency.
- 12. The invention according to claim 8 wherein said one output is high until the <u>frequency</u> of said transducer signal reaches said threshold set <u>frequency</u> whereafter said one output switches low and remains low until the <u>frequency</u> of said transducer signal drops below said reset <u>frequency</u> due to said hysteresis network, and further comprising a transistor in circuit with said starter relay and biased into conduction by said one output when in said high state to enable completion of a circuit through said starter relay whereby the latter may be closed to permit energization of said starter motor and cranking of said engine.
- 15. The invention according to claim 5 wherein said control is a pre-assembled module which may be added to the existing circuitry of a $\underline{\text{vehicle}}$ having an alternator driven by the $\underline{\text{vehicle's}}$ engine:

said module having a first terminal connectable to said battery through said master switch, said first terminal being connected internally of said module to said electronic logic for said main relay, said module having a second terminal connectable to said starter motor, said second terminal being connected internally of said module to one side of said starter relay, said module having a third terminal connectable to said battery in parallel with the series combination of said master switch and said first terminal, said third terminal being connected internally of said module to one side of said main relay, said module having a fourth terminal connectable to said electrical system, said fourth terminal being connected internally of said module to the other side of said main relay, said module having a fifth terminal connectable to

said fourth terminal through said starter switch, said fifth terminal being connected internally of said module to said electronic logic for said starter relay, said module having a sixth terminal connectable to said alternator for feeding to said module an <u>AC</u> signal having a <u>frequency</u> corresponding to engine <u>RPM</u>, said sixth terminal being connected internally of said module to said electronic logic for said starter relay and to said electronic logic for said main relay.

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